

# Robotics I

October 28, 2016

## Exercise 1

Consider the following matrix

$${}^A\mathbf{R}_B(\rho, \sigma) = \begin{pmatrix} \cos \rho & -\sin \rho & 0 \\ \sin \rho \cos \sigma & \cos \rho \cos \sigma & -\sin \sigma \\ \sin \rho \sin \sigma & \cos \rho \sin \sigma & \cos \sigma \end{pmatrix}.$$

- Prove that this is a rotation matrix (representing thus the orientation of a frame  $B$  with respect to a fixed frame  $A$ ) for any value of the pair of angles  $(\rho, \sigma)$ .
- Which is the sequence of two elementary rotations around *fixed* coordinate axes providing  ${}^A\mathbf{R}_B(\rho, \sigma)$ ?
- Which is the sequence of two elementary rotations around *moving* coordinate axes providing  ${}^A\mathbf{R}_B(\rho, \sigma)$ ?
- Verify your statements for  $\rho = 90^\circ$  and  $\sigma = -90^\circ$ .

## Exercise 2

Consider the planar 2R robot in Fig. 1, having link lengths  $\ell_1 = 0.8$  and  $\ell_2 = 0.6$  [m], and let the direct kinematic mapping that characterizes the position of its end-effector be defined as  $\mathbf{p} = \mathbf{f}(\mathbf{q})$ . The motion of this robot is controlled by specifying the joint accelerations  $\ddot{\mathbf{q}}$ .

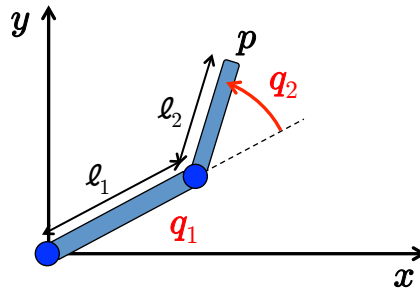


Figure 1: A planar 2R robot.

- What is the expression of the nominal joint acceleration command  $\ddot{\mathbf{q}} = \ddot{\mathbf{q}}_d$  when the robot is in a state  $(\mathbf{q}, \dot{\mathbf{q}})$  and its end-effector needs to move instantaneously with a desired acceleration  $\ddot{\mathbf{p}}_d$ ? Try out your expression by determining the numerical value of  $\ddot{\mathbf{q}}_d$  at the time instant  $t = \bar{t} = 0.8$  [s], when

$$\mathbf{q}(\bar{t}) = \begin{pmatrix} 0 \\ \pi/2 \end{pmatrix} \text{ [rad]}, \quad \dot{\mathbf{q}}(\bar{t}) = \begin{pmatrix} -\pi \\ \pi \end{pmatrix} \text{ [rad/s]}, \quad \mathbf{p}_d(t) = \begin{pmatrix} 0 \\ 0.6(t^3 - 1) \end{pmatrix} \text{ [m]}.$$

- For the same end-effector trajectory specified above, assume now that, at time  $t = 0$ , the robot is in an initial state  $(\mathbf{q}(0), \dot{\mathbf{q}}(0))$  such that  $\mathbf{p}(0) = \mathbf{f}(\mathbf{q}(0)) = \mathbf{p}_d(0)$ , but  $\dot{\mathbf{p}}(0) \neq \dot{\mathbf{p}}_d(0)$ . What should be the expression of the feedback control law for the joint acceleration  $\ddot{\mathbf{q}}$  in order to recover the initial Cartesian trajectory error over time, achieving thus asymptotic trajectory tracking? Define all the needed terms and parameters in this second-order kinematic control law, and determine accordingly the initial numerical value  $\ddot{\mathbf{q}}(0)$  of the control law.

[150 minutes; open books]

# Solution

October 28, 2016

## Exercise 1

It is easy to verify that the given matrix  ${}^A\mathbf{R}_B(\rho, \sigma)$  is a rotation matrix: for any pair  $(\rho, \sigma)$ , its three columns are of unitary norm and orthogonal each to other, while  $\det {}^A\mathbf{R}_B(\rho, \sigma) = +1$ . Moreover, matrix  ${}^A\mathbf{R}_B(\rho, \sigma)$  is obtained as the product of two elementary rotation matrices in the form

$$\mathbf{R}_x(\sigma)\mathbf{R}_z(\rho) = \begin{pmatrix} 1 & 0 & 0 \\ 0 & \cos \sigma & -\sin \sigma \\ 0 & \sin \sigma & \cos \sigma \end{pmatrix} \begin{pmatrix} \cos \rho & -\sin \rho & 0 \\ \sin \rho & \cos \rho & 0 \\ 0 & 0 & 1 \end{pmatrix} = {}^A\mathbf{R}_B(\rho, \sigma).$$

Therefore, it represents

- either a sequence of two rotations around *fixed* axes: first a rotation by  $\rho$  around the  $z$ -axis, and then a rotation by  $\sigma$  around the original  $x$ -axis;
- or, a sequence of two rotations around *moving* axes: first a rotation by  $\sigma$  around the  $x$ -axis, and then a rotation by  $\rho$  around the already rotated  $z$ -axis (i.e.,  $z'$ ).

By substituting  $\rho = \pi/2$  and  $\sigma = -\pi/2$ , we obtain

$${}^A\mathbf{R}_B(\pi/2, -\pi/2) = \begin{pmatrix} 0 & -1 & 0 \\ 0 & 0 & 1 \\ -1 & 0 & 0 \end{pmatrix} = \begin{pmatrix} 1 & 0 & 0 \\ 0 & 0 & 1 \\ 0 & -1 & 0 \end{pmatrix} \begin{pmatrix} 0 & -1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 1 \end{pmatrix} = \mathbf{R}_x(-\pi/2)\mathbf{R}_z(\pi/2).$$

Considering for example the case of moving axes, the first (clockwise) rotation by  $\sigma = -\pi/2$  keeps the  $x$ -axis unchanged,  $\mathbf{x}' \equiv \mathbf{x}$ , while  $\mathbf{y}' \equiv -z$  and  $\mathbf{z}' \equiv \mathbf{y}$ ; the second (counterclockwise) rotation by  $\rho = \pi/2$  keeps the current  $z'$ -axis unchanged,  $\mathbf{z}'' \equiv \mathbf{z}'$ , while  $\mathbf{x}'' \equiv \mathbf{y}'$  and  $\mathbf{y}'' \equiv -\mathbf{x}'$ ; concatenating the two rotations, we obtain  $\mathbf{x}'' \equiv -z$ ,  $\mathbf{y}'' \equiv -x$ , and  $\mathbf{z}'' \equiv \mathbf{y}$ , which is  ${}^A\mathbf{R}_B(\pi/2, -\pi/2)$  as expected.

## Exercise 2

The following piece of Matlab code summarizes the computations needed to answer to the first question:

```
% first question
tbar=0.8;
ddp1=0;ddp2=3.6*tbar;
ddpd=[ddp1;ddp2] % outputs the desired Cartesian acceleration at time t=0.8 s
% current state
q1=0;q2=pi/2;
dq1=-pi;dq2=pi;
dq=[dq1; dq2];
% direct kinematics
p=[l1*cos(q1)+l2*cos(q1+q2);
   l1*sin(q1)+l2*sin(q1+q2)];
% Jacobian matrix
J=[-l1*sin(q1)-l2*sin(q1+q2) -l2*sin(q1+q2);
   l1*cos(q1)+l2*cos(q1+q2)  l2*cos(q1+q2)];
% time derivative of the Jacobian
dJ=[-l1*cos(q1)*dq1-l2*cos(q1+q2)*(dq1+dq2) -l2*cos(q1+q2)*(dq1+dq2);
    -l1*sin(q1)*dq1-l2*sin(q1+q2)*(dq1+dq2) -l2*sin(q1+q2)*(dq1+dq2)];
ddqd=inv(J)*(ddpd - dJ*dq) % outputs the requested joint acceleration command
% end
```

The two resulting outputs of this code are

$$\ddot{\mathbf{p}}_d(0.8) = \begin{pmatrix} 0 \\ 2.88 \end{pmatrix} [\text{m/s}^2], \quad \ddot{\mathbf{q}}_d(0.8) = \begin{pmatrix} 3.6 \\ -16.7595 \end{pmatrix} [\text{rad/s}^2].$$

Similarly, at time  $t = 0$  we request

$$\mathbf{p}_d(0) = \begin{pmatrix} 0 \\ 0.6(t^3 - 1) \end{pmatrix}_{t=0} = \begin{pmatrix} 0 \\ -0.6 \end{pmatrix} [\text{m}]$$

and

$$\dot{\mathbf{p}}_d(0) = \begin{pmatrix} 0 \\ 1.8t^2 \end{pmatrix}_{t=0} = \mathbf{0} [\text{m/s}], \quad \dot{\mathbf{p}}_d(0) = \begin{pmatrix} 0 \\ 3.6t \end{pmatrix}_{t=0} = \mathbf{0} [\text{m/s}^2].$$

The robot should be in an initial state  $(\mathbf{q}(0), \dot{\mathbf{q}}(0))$  such that  $\mathbf{p}(0) = \mathbf{f}(\mathbf{q}(0)) = \mathbf{p}_d(0)$ , but  $\dot{\mathbf{p}}(0) \neq \dot{\mathbf{p}}_d(0)$ . To determine  $\mathbf{q}(0)$ , we solve the inverse kinematics for  $\mathbf{p}_d(0)$ , picking just one of the two solutions (in an arbitrary way):

```
pd0=[0; -0.6];
% second joint computations
c2=(pd0(1)^2+pd0(2)^2-11^2-12^2)/(2*11*12);
s2=sqrt(1-c2^2); %other solution: -sqrt(1-c2^2)
% first joint computations
det=11^2+12^2+2*11*12*c2;
s1=(pd0(2)*(11+12*c2)-pd0(1)*12*s2)/det;
c1=(pd0(1)*(11+12*c2)+pd0(2)*12*s2)/det;
% output
q01=atan2(s1,c1);
q02=atan2(s2,c2);
q0=[q01; q02]
```

We note that the desired Cartesian position is strictly inside the workspace of the 2R robot, so that we are away from kinematic singularities. The output of the above code gives

$$\mathbf{q}(0) = \begin{pmatrix} -2.4119 \\ 2.3005 \end{pmatrix} [\text{rad}] = \begin{pmatrix} -138.19 \\ 131.81 \end{pmatrix} [\text{deg}],$$

yielding no initial Cartesian position error at  $t = 0$ ,  $\mathbf{e}(0) = \mathbf{p}_d(0) - \mathbf{p}(0) = \mathbf{p}_d(0) - \mathbf{f}(\mathbf{q}(0)) = \mathbf{0}$ , as desired. In order to be sure that  $\dot{\mathbf{p}}(0) = \mathbf{J}(\mathbf{q}(0))\dot{\mathbf{q}}(0) \neq \dot{\mathbf{p}}_d(0) = \mathbf{0}$ , we just need to avoid the specific choice  $\dot{\mathbf{q}}(0) = \mathbf{0}$ . For example, by choosing

$$\dot{\mathbf{q}}(0) = \begin{pmatrix} 0.5 \\ 0.1 \end{pmatrix} [\text{rad/s}] \quad \Rightarrow \quad \dot{\mathbf{e}}(0) = \dot{\mathbf{p}}_d(0) - \dot{\mathbf{p}}(0) = -\mathbf{J}(\mathbf{q}(0))\dot{\mathbf{q}}(0) = \begin{pmatrix} -0.3067 \\ -0.0596 \end{pmatrix} [\text{m/s}].$$

To recover any initial Cartesian trajectory error (in velocity and/or position) over time and achieve thus asymptotic trajectory tracking, the control law for the joint acceleration input should be chosen as

$$\ddot{\mathbf{q}} = \mathbf{J}^{-1}(\mathbf{q}) \left( \ddot{\mathbf{p}}_d + \mathbf{K}_d(\dot{\mathbf{p}}_d - \mathbf{J}(\mathbf{q})\dot{\mathbf{q}}) + \mathbf{K}_p(\mathbf{p}_d - \mathbf{f}(\mathbf{q})) - \dot{\mathbf{J}}(\mathbf{q})\dot{\mathbf{q}} \right),$$

with (symmetric) gain matrices  $\mathbf{K}_p > 0$ ,  $\mathbf{K}_d > 0$  (a PD feedback action). By choosing for instance

$$\mathbf{K}_p = 100 \cdot \mathbf{I}_{2 \times 2}, \quad \mathbf{K}_d = 20 \cdot \mathbf{I}_{2 \times 2},$$

we finally obtain at time  $t = 0$

$$\ddot{\mathbf{q}}(0) = \begin{pmatrix} -9.8614 \\ -2.2639 \end{pmatrix} [\text{rad/s}^2].$$

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